

Tight Focusing Properties of Phase Modulated Longitudinally Polarized Doughnut Gaussian Beam

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ABSTRACT: We investigated the focusing properties of a phase modulated radially polarized doughnut Gaussian beam by a high numerical aperture (NA) lens based on vector diffraction theory. We observed that our proposed system generates a sub wavelength focal spot of 0.42λ having large uniform focal depth of 5λ . This kind of non diffracting focal segments is called as dark channel, which may have application in atom trapping, nanolithography, trapping and manipulating particles.

KEYWORDS: Radially polarized beam, Vector Diffraction theory, Doughnut gaussian beam, Optical Trapping.

DOI: 10.29294/IJASE.4.3.2018.651-655

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1. INTRODUCTION

Recently, research on longitudinally polarized laser beams has become a very hot topic due to its potential applications in various areas, such as particle acceleration [1], second harmonic generation [2], fluorescent imaging [3], optical data storage [4] and optical trapping [5]. A radially polarized beam can be focused to generate a strong longitudinal electric field at the focal plane, resulting in a focal spot sharper than that for a linearly polarized beam [6,7]. In theory, a radially polarized Bessel-Gauss beam is focused with a binary optical element and a high numerical aperture (NA) objective to produce a sub-wavelength longitudinally polarized light needle with a depth of focus (DOF) about 4λ [8]. Subsequently, several approaches, such as a narrow width annular beam [9], dual-beam focusing [10] and higher-order beams [11–13], have been employed to realize smaller focal spot sizes and longer DOF. It is of great importance to design the diffractive optical element (DOE) efficiently and accurately. Much work has been done to realize the desired goal methods of designing DOE [14–22,23]. Huang et al [24] formulated a method that combines the global-search-optimization (GSO) algorithm and the tight focusing properties of radially polarized light to design a DOE.

However, to the best of our knowledge, most of the previous research has dealt with beams with either the uniform [25,26] or Laguerre-Gaussian pupil apodization functions [25,27,28]. There has been hardly any investigation of incident beams with Gaussian and Bessel-Gaussian pupil apodization functions, much less a comparison of the optical shaping generated from these beams. Wang et al [29] proposed the double-mode radially polarized (RP) beams can be generated conveniently. But the vector beams possess a uniform pupil apodization

function; therefore, the corresponding optical shaping formed by those vector beams belongs to the case of uniform apodization pattern [25]. In fact, not only can double-mode vector beams with uniform pupil apodization functions be conveniently generated with that approach but so can Laguerre-Gaussian (LG), and Bessel-Gaussian (BG) beams as long as we replace the original computer-generated phase hologram with a new one that carries information of both suitable phase and corresponding amplitude. Having known the different properties of different pupil apodization functions in the case of not only propagation but also tight focusing [30], the optical shaping generated from the LG, the Gaussian, and the BG beams are assumed to show some novel properties. Therefore, a new kind of phase modulated radially polarized beam called doughnut Gaussian (DG) beam is introduced in a high NA focusing system. The defined DG beam is similar to a hollow Gaussian beam. In 2010, a sub-wavelength focal spot was achieved by using a radially polarized narrow-width annular beam [31]. The DG beam, which is similar to the narrow-width annular beam, is falling to the category of the Gaussian beams [32]. Considering that the intensity is null at the center of the doughnut beam, the focusing field of a radially polarized DG incident beam through a high NA lens will exhibit high resolution. In this article, we demonstrate the focusing performance of a longitudinally polarized doughnut gaussian beam with high NA focusing system.

2. Principle of the optical focusing system

A schematic diagram of the suggested method is shown in Fig.1. The longitudinally polarized doughnut Gaussian beam is focused through a multi belt binary phase filter (MBBPF) and is subsequently focused by a high NA lens. The analysis was performed on the basis of Richards and

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Received: 19.02.2018

Accepted: 25.02.2018

Published on: 20.03.2018

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International Journal of Advanced Science and Engineering

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Wolf's vectorial diffraction method [33] widely used for high-NA lens system at arbitrary incident polarization. In the case of the incident polarization, adopting the cylindrical coordinates r, z, φ and the notations of Ref. [34], The focal field of a radially polarized doughnut Gaussian beam (RPDGB) can be written as

$$\vec{E}(r, z) = E_r \vec{e}_r + E_z \vec{e}_z \quad (1)$$

Where E_r and E_z are the amplitudes of the two orthogonal components \vec{e}_r and \vec{e}_z are their corresponding unit vectors.

The two orthogonal components of the electric field is given as

$$E_r(r, z) = A \int_0^\alpha \cos^{1/2}(\theta) T(\theta) \sin 2\theta J_1(kr \sin \theta) e^{ikz \cos \theta} d\theta \quad (2)$$

$$E_z(r, z) = 2iA \int_0^\alpha \cos^{1/2}(\theta) T(\theta) \sin^2 \theta J_0(kr \sin \theta) e^{ikz \cos \theta} d\theta \quad (3)$$

Where $k = 2\pi/\lambda$ is the wave number and $J_n(x)$ is the Bessel function of the first kind with order n . r and z are the radial and z coordinates of observation point in focal region, respectively. $T(\theta)$ describe the amplitude modulation. For a high NA lens, the electric field of the DG beam at the output pupil is defined as follows

$$T(\theta) = \exp \left[- \left(\frac{\sin(\theta) - \theta_0}{\omega_0} \right)^2 \right] \quad (4)$$

where ω_0 reflects the beam size at the beam waist of the Gaussian beam. θ_0 relates with the radius of the DG beam. θ is the variable of the function. Obviously, the shape of the defined doughnut Gaussian beam is determined by θ_0 and ω_0 . To be more specific, the position of the maximum field intensity depends on θ_0 . For $\theta_0=0$ the beam governed by Eq. (4) is a conventional Gaussian beam. The width of the DG beam is determined by ω_0 [35]. The effect of four belt binary phase filter on the input radially polarized doughnut Gaussian beam is evaluated by replacing the function $T(\theta)$ by $T(\theta)BPF(\theta)$. Where $BPF(\theta)$ is given by

$$BPF(\theta) = \begin{cases} 1, & \text{for } 0 < \theta < \theta_1, \theta_2 < \theta < \theta_3, \\ -1, & \text{for } \theta_1 < \theta < \theta_2, \theta_3 < \theta < \theta_{\max} \end{cases} \quad (5)$$

Specially designed optical element has set of four angles. The set of four angles are optimized by traditional global-search-optimization algorithm. Based on this algorithm we choose one structure with random values for θ_1 to θ_3 from all possibilities and simulate their focusing properties by vector diffraction theory. If the structure generates a sub wavelength single or multiple focal holes and satisfies the limiting conditions that that the FWHM of the generated focal spot segment is less than 0.5λ , it is

chosen as the initial structure during the optimization procedures.

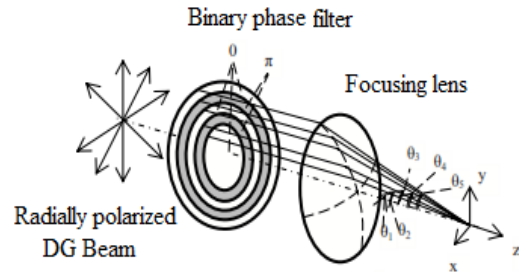


Fig.1. Schematic diagram of the proposed system radially polarized doughnut Gaussian beam passes through a multi belt binary phase filter and is subsequently focused by a high-NA lens

In the following steps, continue to vary θ of one chosen zone to generate a single or splitted focal spots on axial focal field until the generation of uniform intensity on axial profile without affecting the limiting condition. Basing on the above equations, focusing properties of radially polarized DGB with binary phase plate can be investigated theoretically.

3. RESULTS AND DISCUSSION

We performed the integration of Eq. (1) numerically for $NA=0.95$ and $\lambda=1$, $\alpha=\arcsin(NA)$, $\theta_0=0.8$ for all calculation in the length unit is normalized to λ and the energy density is normalized to unity. In order to understand focusing properties of the phase modulated radially polarized doughnut Gaussian beam extensively, firstly, the focusing of radially polarized doughnut Gaussian beam with high NA lens system is investigated without phase

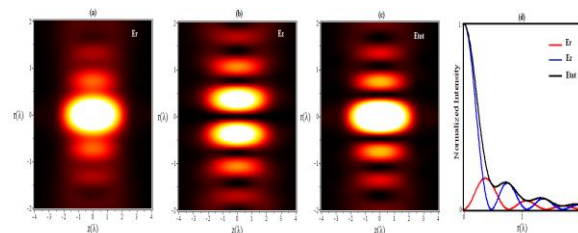


Fig.2. The contour plots of the plane radially polarized doughnut gaussian beam focused by high NA lens. The intensity profiles of the (a) radial, (b) azimuthal and (c) total intensity distribution components of the optical field at near the focus d) 2D intensity distribution for $NA=0.95$ and $\theta_0=0.8$.

modulation. Fig.2(a-c) illustrates the evolution of three-dimensional intensity distribution of radial component, azimuthal component and total intensity of the high NA lens in $r-z$ plane for incident radially polarized doughnut

Gaussian beam (DGB). From Fig. 2d and 2c we measured the radial component is 20% of the total intensity and full width half maximum (FWHM) of the generated focal spot as 0.64λ and its focal depth as 1.4λ respectively. Such a focal spot segment is useful for high refractive index particle trapping.

To realize a relatively long longitudinal polarized light needle with uniform intensity and a narrower spot size, a four belt binary phase optical element is introduced into the optical focusing system. We observed that it is possible to generated sub wavelength focal spot segment by properly tuning the phase of incident radially polarized DG beam using a four belt binary phase filter (BPF). We choose one structure with random values for θ_1, θ_3 from all possibilities and simulate their focusing properties by vector diffraction theory. Fig. 3(a) shows the generation of large focal depth of single sub-wavelength longitudinal focal spot segment generated by the high NA lens for the MBBPF with $\theta_1=16.56^\circ, \theta_2=43.93^\circ, \theta_3=62.28^\circ, \theta_{max}=71.84^\circ$ for $\theta_0=0.8$. It is observed from the Figure 3(a) shows the intensity profile of the radial, longitudinal and total electric field components of the optical field at focus.

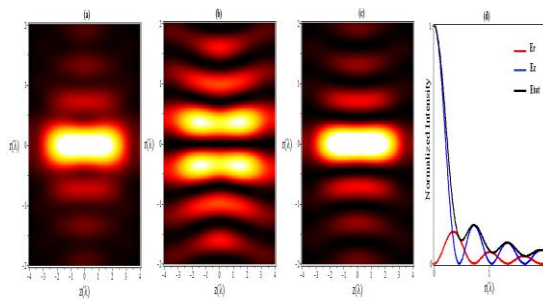


Fig. 3 The contour plots of the phase modulated radially polarized doughnut Gaussian beam focused by high NA lens. The intensity profiles of the (a) radial, (b) azimuthal and (c) total intensity distribution components of the optical field at near the focal plane, (d) 2D intensity distribution for $\theta_0=0.8$.

It is evident that the intensity of the longitudinal component (blue line) is higher than the radial component (red line). From the Fig. 3d, measured the intensity distribution of radial component is only 11% of the normalized total intensity and hence the generated beam is strongly polarized in the longitudinal direction and the FWHM of the generated focal spot is 0.42λ and focal depth of 5λ which is shown in Fig.3(c). Such a needle of sub wavelength longitudinal polarized beam with long focal depth finds its application in near field optical recording and particle acceleration. The depth of focus (DOF) of the focal spot generated by our method extends over two times than that mentioned in recent papers [36-39]. This result is also better than other methods mentioned before. Table 1 shows the comparison of FWHM of the focal spot and its corresponding focal depth generated by the high NA lens system under different methods.

Table .1 Shows that the comparisons of spot size & depth focus for different methods

Methods	Spot size	Depth of focus
Plane DG beam	0.64λ	1.4λ
Five belt binary optics method [36]	0.43λ	$\sim 4\lambda$
Annular beam method [37]	0.43λ	$\sim 4\lambda$
Four Belt binary optics method [38]	0.44λ	$\sim 4\lambda$
Three belt binary [39]	$\sim 0.44\lambda$	$\sim 2\lambda$
Proposed method	0.42λ	5λ

Hence in order to achieve multiple trapping, we suggested a MBBPF optimized with angles are $\theta_1=16.56^\circ, \theta_2=43.93^\circ, \theta_3=62.28^\circ, \theta_{max}=71.84^\circ$. These angles are optimized based on the above-mentioned method but with the limiting condition that the FWHM of the generated focal spot segment is less than 0.5λ , and there should be at least two such focal spots in the focal segment. We observed from the Fig.4(d&c), it is possible to generated series of splitted focal spot each having FWHM of 0.72λ and DOF is 1.8λ and are axially separated by a distance of 4.4λ . Further we measured the radial component is 40% of the total intensity is shown in Fig.4(d). The parameter need to obtain this profile are $\theta_0=0.7$. Such a focal splitting is useful in controlling the position of the optical traps. The above simulation calculations show that, by utilizing the BPF to modulate the phase of radially polarized doughnut gaussian beam (RPDGB), the optical spot in the focal region can be used as a powerful tool for particle manipulation [40-42].

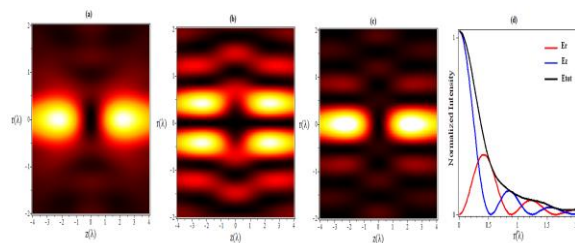


Fig.4. Formation of an splitted focal spots in the $r-z$ plane after a specially designed four-belt phase filter. (a) longitudinal component (b) radial component (c) The total intensity distribution. (d) 2D intensity distribution for $\theta_0=0.7$.

4. CONCLUSION

In conclusion, the proposed multi belt binary phase modulation scheme with high NA lens for the incident radially polarized doughnut Gaussian beam to generated a needle of longitudinally polarized beam with long focal depth (5λ) and sub wavelength focusing (0.42λ) is analyzed and demonstrated numerically by using vector diffraction theory. Apart from generating single focal spot with long depth of focus, we have also showed the possibility of generated splitted focal spot segments

trough properly designed multi belt binary phase filter with radius of the DG beam. These kind of focal spots have been used to optical trapping, the material processing technologies, optical recording, and optical trapping of high refractive index particle.

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